

The Maximum Operating Region in SiGe HBTs for RF Power Amplifiers

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Abstract — Microwave waveforms of SiGe HBTs have been directly measured. The maximum operating region has been experimentally investigated by sweeping the load lines and power of the input signal. The device is found to operate beyond the conventional BV_{ceo} , while GaAs HBTs cannot survive at that voltage. The conventional BV_{ceo} is found to limit the average V_c of the maximum load lines, but has no influence on the peak voltage. Another BV_{ceo} measured with a voltage generator is proposed to represent the avalanche breakdown instead of the conventional one.

I. INTRODUCTION

Recently, SiGe HBTs are going to be used in power amplifiers for mobile communication handsets. The device tends to be used at the high voltage of charging battery and standing waves from mismatched antennas. As the breakdown voltage of the SiGe HBT is relatively lower than that of the GaAs HBT, the maximum operating region of the SiGe HBT is definitely required for the design of the power amplifier. Recent SiGe power amplifiers can operate at a high collector voltage near the breakdown voltage [1-3]. Some of them can even survive at the high VSWR condition [3]. On the other hand, GaAs HBT amplifiers can operate at nearly one-third of the breakdown voltage [4].

Failure mechanisms and thermal instability in GaAs and SiGe HBTs were studied under DC

conditions. However, these thermal condition and electric fields are completely different from the real microwave operation of the device, since physical time constants are not considered in the DC operation. To overcome this problem, the operating limits in a GaAs HBT were investigated by the direct measurement of the microwave waveforms [5]. However, no direct waveform measurement in SiGe HBTs near the operating limits has been reported.

In this study, the real current and voltage waveforms of SiGe HBTs at 0.9GHz have been directly measured. By sweeping load lines and input power P_{in} , the maximum operating region has been experimentally investigated. The relation between the conventional BV_{ceo} and microwave limits are also discussed.

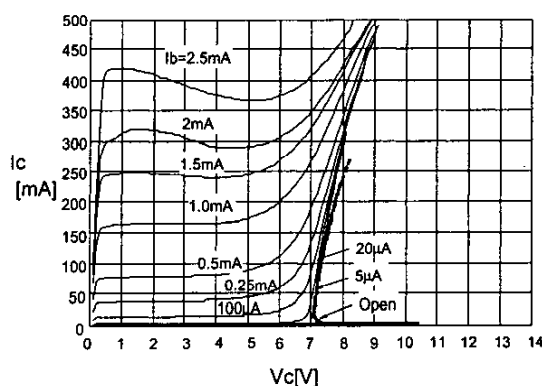


Fig.1 IV characteristics of the SiGe HBT with a constant I_b .

II. MEASUREMENT

A SiGe high power HBT is measured in the common-emitter configuration. The emitter area is $2 \times 30 \mu\text{m}^2 \times 240$ -fingers. Figure 1 shows the measured DC-IV characteristics of the HBT with a constant I_b . The bold line in the figure denotes the collector current measured by a current generator with opened base. The conventional BV_{ceo} is 7.0V.

In order to investigate the maximum operating region at the microwave frequency, the incident and reflected waves at the base and collector terminals are measured using a microwave transition analyzer up to 18GHz. The current and voltage waveforms at the transistor are calculated from the full-two-port calibration data [6]. The input and output matchings are adjusted to getting the proper load lines using automated tuners. The microwave waveforms at the pads of the device are calculated using the measured S-parameters of the test fixture.

To find the maximum collector voltage (V_c) with each collector current (I_c), we gradually increased the V_c while maintaining the I_c by V_b adjustment. The load contours were measured until the HBT reached its operating limits. These measurements were performed for several I_c and P_{in} values. The source and load impedances were fixed during these measurements.

III. RESULTS

With the small P_{in} of 12.0dBm, we performed the waveform measurement procedure described in the previous section. Figure 2 shows all the load lines just before reaching its operating limits. Therefore, these lines represent the maximum operating region of the device with this specific input power, source and load impedances.

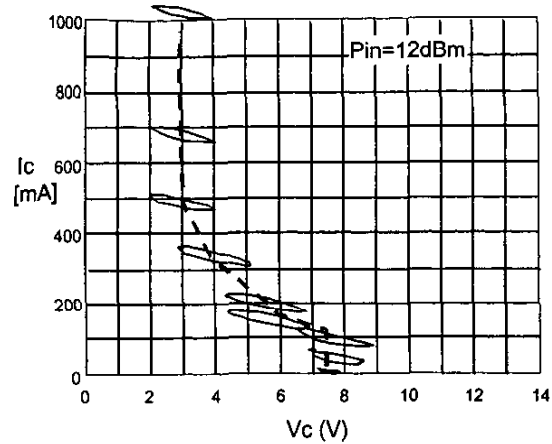


Fig.2 Measured maximum load lines with the P_{in} of 12.0dBm and the average $I_c V_c$ of the load lines (dotted line).

An increase in the V_c beyond these lines results in two modes. One is a runaway of the collector current in the high collector current region over 100mA, and the other is an unstable operation in the low I_c region, where the average base current decreases to negative. The SiGe HBT can survive at this negative base current operation, while the GaAs HBT rushes into burnout. However, it is unstable and goes to burnout at a higher collector voltage. We defined this limit at the V_c where I_b becomes negative.

The dotted line in the figure denotes the average V_c and I_c at the maximum load lines. In the low I_c region under 100mA, the average V_c is almost same as the BV_{ceo} . Furthermore, the peak voltage exceeds the breakdown voltage. This is different from the GaAs HBT, in which the peak voltage cannot go over the BV_{ceo} .

As the base bias is supplied by a constant voltage source, these limits at a small RF power are supposed to be related to the DC limits with constant base voltage. Figure 3 shows the IV characteristics with a constant V_b condition. The dotted line denotes the average $I_c V_c$ of the maximum load lines in Fig.2. The dotted line shows good agreement with the values of thermal

runaway in the DC IV curve. Therefore, the average V_c and I_c of the load lines dominate the limits with the P_{in} of 12dBm.

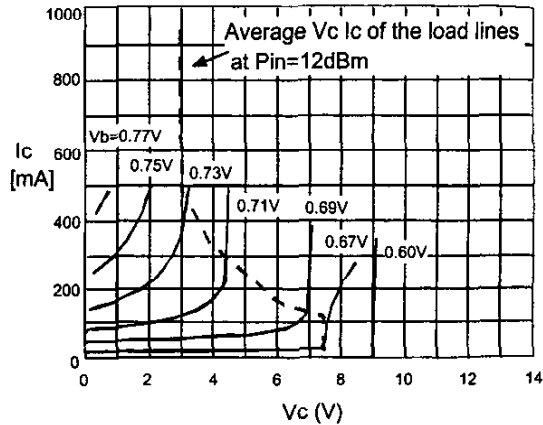


Fig.3 IV characteristics with a constant V_b (solid line) and the average V_c I_c of the maximum load lines at the P_{in} of 12.0dBm (dotted line).

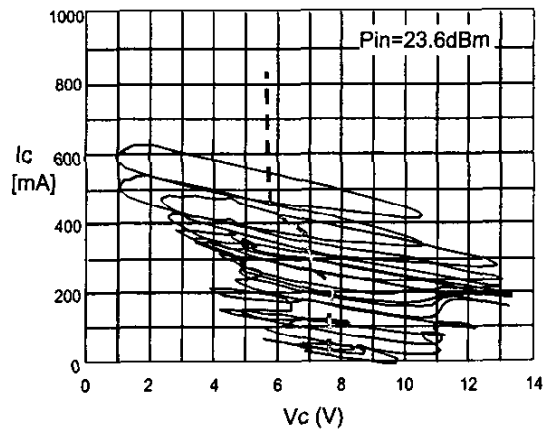


Fig.4 Measured maximum load lines with the P_{in} of 23.6dBm and the average I_c V_c of the lines (dotted line).

In order to confirm this explanation, the same measurement with larger input power P_{in} 's of 18dBm and 23.6dBm were performed. Figure 4 shows the

measured load lines with the P_{in} of 23.6dBm. The peak collector voltage goes far beyond the BV_{ceo} , while the average V_c still remains at 7.5V. The peak and average collector voltages are summarized in Fig.5. The solid lines are the envelope of the peak V_c of all the maximum load lines. The dotted lines show the average V_c I_c values of the load lines. The gray lines denote the IV characteristics in Fig.3. In the high I_c region, the average V_c increases with larger P_{in} . This means that the SiGe HBT can also operate beyond the DC thermal limit with a large P_{in} . This phenomena is similar to that of the GaAs HBT. However, the average V_c is restricted by the BV_{ceo} , because its bias cannot be set over the BV_{ceo} due to the thermal runaway.

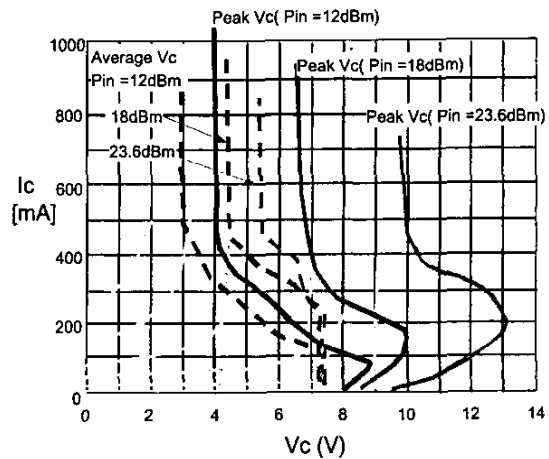


Fig.5 The envelope of the peak and average V_c of the maximum load lines with P_{in} values of 12, 18 and 23.6dBm.

As for the peak V_c , most of them exceed the BV_{ceo} . The peak V_c at a P_{in} of 23.6dBm reaches 13.1V. For this SiGe HBT, the BV_{ceo} has no influence on the peak V_c . This is different from the GaAs HBT.

This difference is explained as follows. Usually, the BV_{ceo} is measured using a current generator. As shown in the bold line in Fig.1, the peak voltage of 10.8V was observed before V_c goes into the

conventional BV_{ceo} with a larger I_c . This means that an avalanche breakdown occurs around 10.8V. Also, the following impact ionization induces thermal runaway which reduces V_c to 7V. Thus, this BV_{ceo} of 7.0V shows its thermal limits, not the avalanche breakdown. Generally, the avalanche breakdown is considered to affect the peak voltage because its time constant is very fast. On the contrary, the thermal runaway has no influence on the microwave operation due to its slow time constant.

Based on this explanation, the conventional BV_{ceo} is not adequate to represent the peak voltage limit from the avalanche breakdown. We then measured BV_{ceo} with a voltage generator by sweeping the V_c , because no reduction in the V_c occurs after the avalanche breakdown. With this method, the BV_{ceo} of 13.0V is obtained. This agrees with the peak voltage of the measured load lines around 200mA at the Pin of 23.6dBm.

IV. CONCLUSIONS

The load and source waveforms of the SiGe HBT at 0.9GHz have been directly measured using a microwave waveform measurement system. The maximum operating region has been experimentally examined. Under a small input power operation, the average V_c I_c of the maximum load lines are determined by the DC thermal runaway condition. With a large input power, the HBT is found to operate beyond the DC limit of thermal runaway similar to the GaAs HBT. The device is also found to operate beyond the conventional BV_{ceo} where the GaAs HBT cannot survive. The conventional BV_{ceo} is considered to show the thermal limits, not the avalanche breakdown that affects the peak voltage. Instead of the conventional BV_{ceo} , the BV_{ceo} measured with a voltage source is suitable for the peak voltage limit. These results contribute to the design of SiGe high power amplifiers.

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